J. Szantyr – Lecture No. 12 – Energy conservation equation

Kinetic energy of the fluid may be treated as the sum of the macroscopic motion energy and molecular motion energy or internal energy: $\int_{V} \left(\frac{u^2}{2} + e \right) dV \qquad \overline{u} \left(u_x, u_y, u_z \right) \qquad u = \left| \overline{u} \right|$

Rate of change (i.e. material derivative) of the total kinetic energy of the fluid volume *V* surrounded by the fluid surface *S* is equal to the sum of the power of mass forces, the power of surface forces and the stream of energy (heat) supplied to the element.

- \overline{j} stream of supplied energy (heat) $\overline{j}(j_x, j_y, j_z)$
- \overline{n} External unit normal vector

where:

The surface integrals in this equation may be converted into the volume integrals. If simultaneously we express the unit surface forces by the stress tensor $[\mathbf{P}]$, the above equation may be converted into the following form:

$$\int_{V} \left[\rho \frac{D}{Dt} \left(\frac{u^{2}}{2} + e \right) - \rho \bar{f} \bullet \bar{u} - div \left(\left[P \right] \bar{u} \right) + div \bar{j} \right] dV = 0$$

As the volume of integration is arbitrarily selected, the function under the integral must be also equal to zero, what leads to the integral form of the energy conservation equation:

$$\rho \frac{D}{Dt} \left(\frac{u^2}{2} + e \right) = \rho \overline{f} \bullet \overline{u} + div \left(\left[P \right] \overline{u} \right) - div \overline{j}$$

Full development of the operators in the equation leads to the following form:

$$\rho \frac{D}{Dt} \left(\frac{u^2}{2} + e \right) = \rho \left(f_x u_x + f_y u_y + f_z u_z \right) + \frac{\partial}{\partial x} \left[(-p + \tau_{xx}) u_x + \tau_{yx} u_y + \tau_{zx} u_z \right] + \frac{\partial}{\partial y} \left[\tau_{xy} u_x + (-p + \tau_{yy}) u_y + \tau_{zy} u_z \right] + \frac{\partial}{\partial z} \left[\tau_{xz} u_x + \tau_{yz} u_y + (-p + \tau_{zz}) u_z \right] + \frac{\partial}{\partial z} \left[\tau_{xz} u_x - \frac{\partial j_x}{\partial y} - \frac{\partial j_z}{\partial z} \right]$$

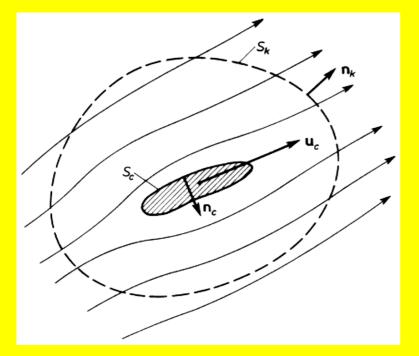
If the field of mass forces is a stationary potential field such that $\bar{f} = -grad\Pi$ then the energy conservation equation may be written as:

$$\rho \frac{D}{Dt} \left[\left(\frac{u^2}{2} + e + \Pi \right) \right] = div ([P]\overline{u}) - div\overline{j}$$

or in the form of an integral equation:

$$\int_{V} \frac{\partial}{\partial t} \left[\rho \left(\frac{u^{2}}{2} + e + \Pi \right) \right] dV + \int_{S(V)} \rho \left(\frac{u^{2}}{2} + e + \Pi \right) u_{n} dS = \int_{S(V)} \overline{\tau} \bullet \overline{u} dS - \int_{S(V)} \overline{j} \bullet \overline{n} dS$$

Example No. 1: the case of an external flow around a body



- S_k the control surface
- u_c the velocity of the body

The energy conservation equation for such a case has the form:

$$\int_{V(S_{k}-S_{c})} \frac{\partial}{\partial t} \left[\rho \left(\frac{u^{2}}{2} + e + \Pi \right) \right] dV + \int_{S_{k}} \rho \left(\frac{u^{2}}{2} + e + \Pi \right) u_{n} dS_{k} + \int_{S_{c}} \rho \left(\frac{u^{2}}{2} + e + \Pi \right) u_{n} dS_{c} =$$
$$= \int_{S_{k}} \overline{\tau}_{nn} \bullet \overline{u} dS_{k} + \int_{S_{k}} \overline{\tau}_{nt} \bullet \overline{u} dS_{k} + \int_{S_{c}} \overline{\tau}_{nn} \bullet \overline{u} dS_{c} + \int_{S_{c}} \overline{\tau}_{nt} \bullet \overline{u} dS_{c} - \int_{S_{k}} \overline{j} \bullet \overline{n}_{k} dS_{k} - \int_{S_{c}} \overline{j} \bullet \overline{n}_{c} dS_{c}$$

As the body surface is impermeable, the third term on the left hand side is equal zero. Moreover, if the velocity \overline{u}_c is the same in all points of the body, we may write:

$$\int_{S_c} \overline{\tau}_{nn} \bullet \overline{u}_c dS_c + \int_{S_c} \overline{\tau}_{nn} \bullet \overline{u}_c dS_c = \overline{u}_c \left[\int_{S_c} \overline{\tau}_{nn} dS_c + \int_{S_c} \overline{\tau}_{nt} dS_c \right] = -\overline{u}_c \bullet \overline{R}$$

where *R* is the hydrodynamic reaction force acting on the body.

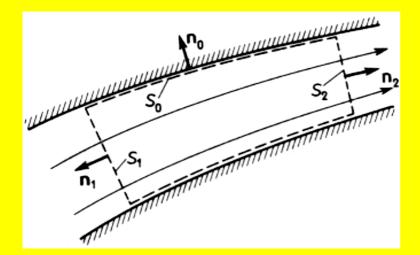
If we also assume:

$$\frac{\partial}{\partial t} = 0 \quad \overline{j} = 0 \quad \overline{\tau}_{nt} = 0 \quad \overline{\tau}_{nn} = -p\overline{n}$$
we obtain:

$$\overline{u}_{c} \bullet \overline{R} = -\int_{S_{k}} \rho \left(\frac{u^{2}}{2} + e + \frac{p}{\rho} + \Pi\right) u_{n} dS_{k}$$

Conclusion: the hydrodynamic force acting on a body may be determined through the analysis of the hydrodynamic wake behind this body, without the direct measurement e.g. by means of a dynamometer.

Example No. 2: the case of internal flow (flow in a channel)



Assumption: the flow is stationary.

The energy conservation equation for such a case has the form:

$$m\left[\left(\frac{\tilde{u}^{2}}{2}+\tilde{e}+\tilde{\Pi}\right)_{S_{2}}-\left(\frac{\tilde{u}^{2}}{2}+\tilde{e}+\tilde{\Pi}\right)_{S_{1}}\right]=\int_{S_{0}}\bar{\tau}_{nn}\bullet\bar{u}dS_{0}+\int_{S_{0}}\bar{\tau}_{nt}\bullet\bar{u}dS_{0}+\int_{S_{1}}\bar{\tau}_{nn}\bullet\bar{u}dS_{1}+\int_{S_{1}}\bar{\tau}_{nn}\bullet\bar{u}dS_{2}+\int_{S_{2}}\bar{\tau}_{nt}\bullet\bar{u}dS_{2}-\int_{S_{0}}\bar{j}\bullet\bar{n}_{0}dS_{0}-\int_{S_{1}}\bar{j}\bullet\bar{n}_{1}dS_{1}-\int_{S_{2}}\bar{j}\bullet\bar{n}_{2}dS_{2}$$

m – mass intensity of flow

The left hand side of the equation contains mean values defined in the following way:

$$\left(\frac{\tilde{u}^2}{2} + \tilde{e} + \tilde{\Pi}\right)_S = \frac{1}{m} \int_S \rho \left(\frac{u^2}{2} + e + \Pi\right) u_n dS$$

Additional assumptions:

-the fluid is inviscid, so the tangential stresses are zero and the normal stresses are expressed only by pressure,

-There is no heat transport through the inlet and outlet surfaces.

This leads to the expression: where: $\Pi = gz$

$$m\left[\left(\frac{\tilde{u}^2}{2} + \tilde{e} + \frac{\tilde{p}}{\tilde{\rho}} + \tilde{\Pi}\right)_{S_1} - \left(\frac{\tilde{u}^2}{2} + \tilde{e} + \frac{\tilde{p}}{\tilde{\rho}} + \tilde{\Pi}\right)_{S_2}\right] = -\int_{S_0} \bar{j} \cdot \bar{n}_0 dS_0$$

This expression may describe for example the flow through the pipe in a heat exchanger.